

Hypothetical Gravity Control and Possible Influence on Space Propulsion

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In nearly all concepts invoked or proposed to change or shield gravity it is intuitively assumed that manipulation of gravity automatically leads to a breakthrough for propulsion. In this study it is shown that even if gravity hypothetically could be controlled according to the manipulation schemes outlined, the gains in terms of propulsion would be modest and lead to no breakthrough. Although the manipulation schemes presented are not exhaustive, they include the most straightforward ones from the current physics point of view.

Nomenclature

c	=	speed of light = $3 \times 10^8 \text{ m} \cdot \text{s}^{-1}$
F	=	force
G	=	gravitational constant = $6.67 \times 10^{-11} \text{ m}^3 \cdot \text{kg}^{-1} \cdot \text{s}^{-2}$
g_0	=	standard gravitational acceleration = 9.81 ms^{-2}
I_{sp}	=	specific impulse
m_p	=	propellant mass
R	=	universal gas constant = $8.31 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$
T_c	=	combustion chamber temperature
v_p	=	propellant velocity
γ	=	adiabatic index
δ	=	inertial mass modification factor
ε	=	gravitational mass modification factor
μ_p	=	molar propellant mass

Introduction

A S part of its advanced space propulsion program, NASA created the Breakthrough Propulsion Physics Program in 1996 to look for new concepts in propulsion that could ultimately enable interstellar travel.^{1,2} Nearly all concepts proposed involved some method to alter gravity, such as warp drives,³ transient mass fluctuations,^{4,5} or gravitational shielding effects.⁶ They all intuitively assumed without any justification, that manipulation of gravity would automatically lead to a breakthrough for propulsion.

Subsequently, in 2001, the European Space Agency (ESA) funded a study to evaluate the concept of gravity control in light of current theories of gravity and field theory, as well as to assess the scientific credibility of claims in the literature of anomalous gravitational experiments and phenomena.⁷ Furthermore, the study was to analyze the impact on spacecraft propulsion of any degree of gravity control.

As anticipated, the first part of the study yielded no surprises, because current experimental knowledge and bounds on the fundamental underlying principles of general relativity and of the standard model of the fundamental interactions leave little room for the gravity control proposals that were analyzed. Among these we

could mention exotic concepts such as theories where gravity is due to interactions with the zero-point-energy field,^{8,9} warp-drive mechanisms,³ or propulsion concepts based on Mach's principle.^{4,5} None of the approaches examined proved fruitful. However, the second part of the study has turned out to be rather rich in new findings. Our main conclusion was that even if gravity could be controlled or modified, influence on spacecraft propulsion would be quite modest and would not lead to breakthroughs in the conceptual framework of presently known propulsion principles within the studied manipulation schemes. We regard this result as being of particular importance to the breakthrough propulsion physics community and they should, in our opinion, be considered in any further work on the topic.

Gravity Control

Current knowledge of gravitational phenomena is accurately described by Einstein's theory of general relativity. The theory matches all known experimental data. Experimental windows of opportunity can be found in the untested ground of gravity-like forces below the millimeter scale or beyond 10^{14} km , or in violations of the weak equivalence principle for antiparticles. Consistency between quantum mechanics and general relativity, which requires a still elusive quantum gravity theory, leads for instance to the quite novel framework of superstring physics, and this theory may give rise to new effects, such as a deviation from the weak equivalence principle at the 10^{-18} level.¹⁰ The reader is referred to Ref. 7 for an extensive review of these issues (see also Ref. 11).

In addition to changes in inertial or gravitational mass, there is one aspect of general relativity that is more closely related to possible propulsion applications. In the lowest order of the weak field limit, general relativity can be restructured in such a way that it closely resembles Maxwell's equations.¹² In this context, there is a similarity between moving charges and moving masses, to which the classical laws of electromagnetism apply. For instance, a mass in motion generates a gravitational interaction that is similar to a magnetic field, the so-called gravitomagnetic field. This gravitomagnetic field can interact with other gravitomagnetic fields, creating forces.¹³ Such forces are very weak (usually 10^{-20} N or less in Earthlike environments), but can in principle be detected by extremely sensitive gyroscopes such as the ones developed for NASA's Gravity Probe B (GP-B) mission. The frame-dragging effect of the Earth was experimentally measured using the LAGEOS and LAGEOS II laser ranging satellites¹⁴ and is currently being investigated by NASA's GP-B mission.

Induction laws such as the ones encountered in electromagnetism exist in this approximation of general relativity, making possible the conversion of gravitoelectric fields into gravitomagnetic fields and vice versa. Effects related to the gravitomagnetic field are also referred to as frame-dragging or the Lense–Thirring effect.¹² We

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shall analyze the effects for propulsion arising from such forces in more detail in a later section.

In quite general terms, we find that any scheme to hypothetically control gravity must fulfill at least one of the following conditions:

- 1) Existence of a new fundamental interaction of nature to alter the effective strength of the gravitational coupling to matter. This implies violations of the weak equivalence principle.
- 2) Existence of net forces due to the interplay between gravity and electrostatic forces in shielded experimental configurations, as found in the well-known Schiff–Barnhill effect.¹⁵
- 3) An effect analogous to magnetic fields in quantum materials involving the gravitomagnetic field.^{16,17}
- 4) Physically altering the vacuum properties to change the relative strength of known fundamental interactions of nature.

Classical Spacecraft Propulsion and Definition of Terms

All classical propulsion systems rely on Newton's mechanics. Equations characterizing the performance of any propulsion system can be found in a large variety of textbooks, such as Ref. 18. In this section, we will recall basic equations that will be used for the analysis of gravity control.

In general terms, assuming a constant propellant velocity, the force F is defined as

$$F = -|\dot{m}_p|v_p \quad (1)$$

where \dot{m}_p is the propellant mass flow and v_p the propellant velocity. To a good approximation, the specific impulse I_{sp} is proportional to the propellant exhaust velocity. Neglecting the influence of the nozzle or the ambient atmosphere, the propellant velocity for a simple chemical thruster can be written as

$$v_p \cong \sqrt{2\gamma/(\gamma - 1) \cdot RT_c/\mu_p} \quad (2)$$

where γ is the adiabatic index, R the universal gas constant, T_c the temperature in the combustion chamber, and μ_p the molar mass of the propellant. We clearly see that the following scaling laws are valid:

$$F \propto m_p^{\frac{1}{2}}, \quad I_{sp} \propto v_p \propto m_p^{-\frac{1}{2}} \quad (3)$$

Apart from electromagnetic thrusters, these scaling laws also apply for other propulsion systems such as electric thrusters (e.g., Hall, ion, or field emission thrusters) to a good approximation. The amount of propellant needed for a given mission is derived from the trajectory analysis and is typically expressed as the required change of velocity from the spacecraft, Δv . The total requirement consists of several components,

$$\Delta v = \Delta v_g + \Delta v_{orbit} + \Delta v_{drag} - \Delta v_{initial} \quad (4)$$

namely the Δv_g to overcome the gravitational potential (e.g., from the Earth's surface to the required orbit), Δv_{drag} due to drag from the atmosphere (usually around 0.1 km/s), Δv_{orbit} giving the velocity increment to reach a certain orbit, and $\Delta v_{initial}$ the initial velocity (e.g., due to the Earth's centrifugal force, which on the equator is about 0.4 km/s). The following equations are used to characterize the most dominant Δv parts:

$$\Delta v_g = \sqrt{2GM(1/r_{initial} - 1/r_{final})} \quad (5)$$

$$\Delta v_{orbit} = \sqrt{GM/r} \quad (6)$$

where G is the gravitational constant, M the Earth's mass, and r the orbit's distance to the center of the Earth. For example, a low Earth orbit (LEO) of altitude 100 km ($r_{initial} = 6400$ km, $r_{orbit} = 6500$ km) results in $\Delta v_{orbit} = 7.8$ km/s and $\Delta v_g = 1.4$ km/s, starting from Earth's surface. The total requirement would then be $\Delta v_{LEO} = (1.4 + 0.1 + 7.8 - 0.4)$ km/s = 8.9 km/s. The propellant mass necessary to meet the full Δv requirement can be calculated using the well-known Tsiolkovski equation:

$$m_p = m_0 \cdot [1 - \exp(-\Delta v/v_p)] \quad (7)$$

Influence of Gravity Manipulation on Spacecraft Propulsion

In the following discussion we shall consider a series of hypothetical devices capable of manipulating mass (with influence on current propulsion systems) or generating an artificial gravitational field (new propulsion concept using gravity control). As already discussed, no such devices are known. Nevertheless, several combinations (during launch and in space) are going to be analyzed and their influence on propulsion systems or as force generators will be discussed. In order to avoid complexity (we are talking about hypothetical gravity control devices anyhow), we do not endow the gravity control manipulator with any special attributes and do not limit its manipulation to certain distances.

Inertial Mass Modification

Let us assume a device that can change the inertial mass of bodies in its interior, such as a launcher. If the spacecraft were to fire conventional chemical rockets or electric propulsion thrusters how would this device affect performance? We define an inertial mass modification factor δ and introduce it into the equations for the specific impulse and force for chemical thrusters:

$$I_{sp} \propto v_p \cong \sqrt{2\gamma/(\gamma - 1) \cdot RT_c/(\mu_p \cdot \delta)} \propto \delta^{-\frac{1}{2}} \quad (8)$$

and hence

$$F = \delta m_p v_p \propto \delta^{\frac{1}{2}} \quad (9)$$

Notice that these are the same scaling laws previously discussed. Thus, hypothetical inertial mass modification is similar to choosing a propellant with a different molar mass. These laws are similar for all other classical propulsion systems. The only advantage would be that by manipulating inertial mass, the chamber temperature T_c would not really be changing. This might not be the case for choosing a lighter propellant in chemical thrusters (e.g., H_2/O_2 instead of kerosene/ O_2). If T_c is lower, the specific impulse drops as well. Also, the spacecraft mass can be reduced conventionally, e.g., by using lightweight structures. This will then reduce the Δv requirement accordingly—but not affect the propulsion system performance.

How is the Δv requirement influenced? The kinetic energy has now to be multiplied by the factor δ and one derives the modified equations

$$\Delta v_g = \sqrt{2GM(1/r_{initial} - 1/r_{final}) \cdot 1/\delta} \propto \delta^{-\frac{1}{2}} \quad (10)$$

and

$$\Delta v_{orbit} = \sqrt{GM/r \cdot 1/\delta} \propto \delta^{-\frac{1}{2}} \quad (11)$$

Hence, an inertial mass reduction would actually *increase* the Δv requirement! For the extreme case of $\delta = 0$, the launcher would not move any more ($F = 0$) and accordingly the Δv requirement would be infinite. Thus, for $0 < \delta < 1$, thrust F would increase, whereas the specific impulse I_{sp} would decrease (see Fig. 1). This is similar

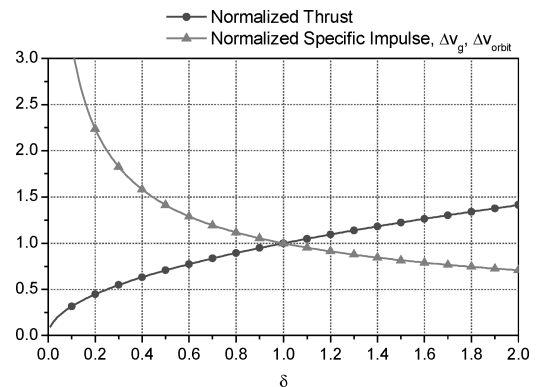


Fig. 1 Influence of inertial mass modification factor δ on propulsion parameters.

to using a heavier propellant, such as solid boosters with alumina oxides instead of H_2/O_2 chemical thrusters.

An interesting result is that Tsiolkovski's Eq. (7) is not affected at all by a modification of the inertial mass. Indeed, to a good approximation one can neglect Δv_{drag} and $\Delta v_{\text{initial}}$ so that the total $\Delta v \propto \delta^{1/2}$. Furthermore, one can see that all δ factors are cancelled out in Eq. (7). Therefore, whatever the inertial mass modification, the amount of propellant will not be changed, or in other words, the change in the propulsion performance is always counterbalanced by the change in the Δv requirement!

We conclude that a modification of the inertial mass is of *no* interest for propulsion.

Gravitational Mass Modification

We turn now to the analysis of the modification of gravitational mass. Such modification does not influence propulsion performance (thrust, specific impulse); only parts of the Δv requirement are affected in this case. By using the gravitational mass modification factor, dividing the gravitational by the inertial mass, $\varepsilon = m_g/m_i$, we get

$$\Delta v_g = \sqrt{2GM\varepsilon(1/r_{\text{initial}} - 1/r_{\text{final}})} \propto \varepsilon^{1/2} \quad (12)$$

and

$$\Delta v_{\text{orbit}} = \sqrt{GM/r \cdot \varepsilon} \propto \varepsilon^{1/2} \quad (13)$$

Neglecting as before Δv_{drag} and $\Delta v_{\text{initial}}$, we obtain $\Delta v \propto \varepsilon^{1/2}$, approximately. The modified Tsiolkovski equation can then be written as

$$m_p = m_0 \cdot \{1 - \exp[-(\Delta v \cdot \varepsilon^{1/2})/v_p]\} \quad (14)$$

If the gravitational mass were reduced, that is, $\varepsilon < 1$, the Δv requirement would drop and less propellant mass would be required. For a satellite orbiting the Earth, our modified definition of Δv_{orbit} in Eq. (13) also increases the time it needs to make a full orbit (less speed to cycle the Earth). This may not be important for launching interplanetary probes, but affects, for instance, remote sensing or geostationary orbit (GEO) satellites which need to cycle Earth with a certain speed for the purpose of mapping and telecommunication. In such cases the full $\Delta v_{\text{orbit}}(\varepsilon = 1)$ would have to be applied with no reduction, which then in turn would cause an unstable orbit, since the centrifugal force would be higher than the gravitational pull. To counterbalance this effect, two different strategies are possible:

1) Launch of the spacecraft with the gravitational mass manipulator (GMM) activated. Once in orbit, GMM would be deactivated and full Δv_{orbit} applied using a propulsion system. The centrifugal force would then be balanced by the gravitational push.

2) GMM always active and propulsion system used to counterbalance the higher centrifugal force to stay in orbit.

As an example, we consider a scientific satellite for a planetary target ($\Delta v = 10$ km/s) with a chemical thruster ($v_p = 3500$ m/s). In this case we do not need a full Δv_{orbit} and our above-mentioned concerns do not apply. In Fig. 2 the Δv and propellant mass ratio (m_p/m_0) reduction are plotted as a function of ε . For $\varepsilon = 0.05$, only half of the propellant would be required. Of course, shielding very close to $\varepsilon = 0$ would reduce the propellant consumption to zero and a very direct trajectory to the target would be possible. Applying Newton's laws, the trip time to reach a required Δv scales with $\varepsilon^{1/2}$. Therefore, shielding of gravitational mass does reduce the trip time; however, even shielding of $\varepsilon = 0.05$ only reduces trip time by a factor of 4.5. In conclusion, unless almost total shielding can be achieved, there is no breakthrough in the overall trip time.

Let us assume the extreme case where the gravitational mass vanishes and thus Δv_g vanishes. The Δv requirement, still including the full Δv_{orbit} for typical LEO satellites, would then change from Eq. (4) to

$$\Delta v = \Delta v_{\text{orbit}} + \Delta v_{\text{drag}} - \Delta v_{\text{initial}} \quad (15)$$

Considering again our previous 100-km LEO example, the case of $\Delta v_g = 0$ would reduce the total Δv requirement from the initial

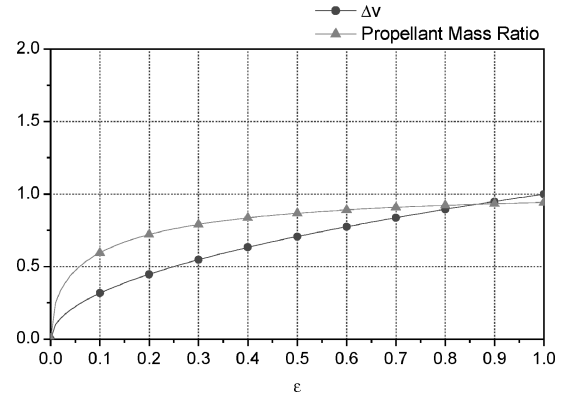


Fig. 2 Influence of gravitational mass modification factor ε on propulsion parameters.

8.9 km/s by 1.4 km/s, that is, down to 7.5 km/s. So a launcher, although with less propellant, would still be required. The higher the original Δv_g , the higher the possible reduction of the total Δv . GEO satellites with a high altitude of 42,160 km could reduce in this case from a total Δv of about 13 km/s to 3 km/s, which would require a much smaller propulsion system, reducing launch costs drastically. Only in the case where Δv_{orbit} is not important, as in, for example, interplanetary spacecraft, we can assume a full reduction to

$$\Delta v = \Delta v_{\text{drag}} - \Delta v_{\text{initial}} \quad (16)$$

If the spacecraft is close to the equator, then $\Delta v_{\text{initial}} \approx 0.4$ km/s from the spinning Earth is higher than $\Delta v_{\text{drag}} \approx 0.1$ km/s and so it would start lifting by itself. That could lead to completely new launch strategies and would certainly be a breakthrough.

How far away are we from such a possible breakthrough? The experimental verification of the Weak Equivalence Principle indicates that $\varepsilon = 1 \pm 5 \times 10^{-13}$. On the other hand, string theory predicts¹⁰ that $\varepsilon = 1 \pm 1 \times 10^{-18}$. Obviously, these values do not influence propulsion at all. As previously outlined, significant deviations from $\varepsilon = 1$ are not foreseen, unless, for instance, the behavior of antiparticles in a gravitational field is substantially different from that of particles.

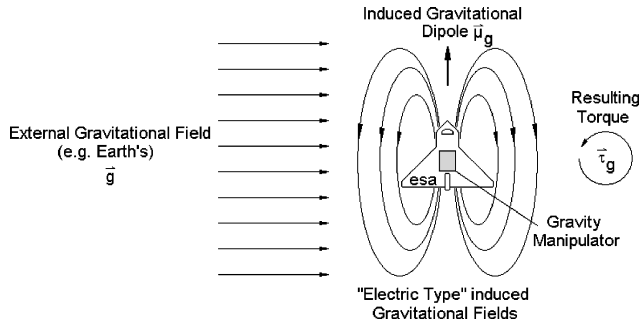
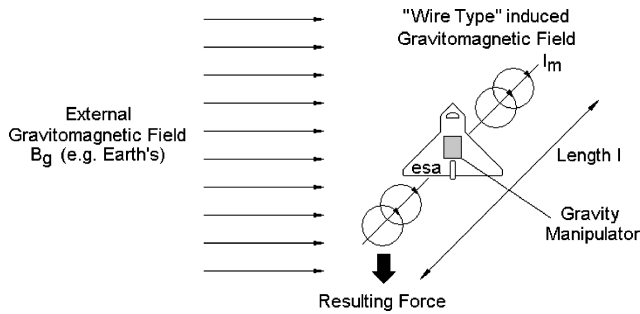
Even if situations where $\varepsilon \neq 1$ can be engineered, they would have to compete with concepts such as electric propulsion, which can already lower the propellant consumption by 90% with much higher propellant velocities. There are also technologies and concepts available that can reduce the Δv requirement and trip time. One example is to reduce the gravitational potential Δv_g simply by launching from a mountain or to supply a higher initial velocity $\Delta v_{\text{initial}}$ by launching from an airplane (e.g., the Pegasus rocket from Orbital Sciences Corporation is currently being launched from an aircraft to reduce of the Δv requirement). NASA, for instance, is developing an initial acceleration rail for future spacecraft that uses superconducting magnetic levitation (MAGLIFTER); the rocket engine is fired after the spacecraft reaches a speed of 300 m/s. For an extreme summary of launch assist technology, see Ref. 19. An extreme concept was put forward by Arthur C. Clarke,²⁰ who proposed to build an ultrahigh tower, which was named a space elevator, for lifting spacecraft to orbits as high as 100 km.

Dipolar Gravitoelectric Field

The possibility of generating artificial gravitational fields would make possible new concepts for space propulsion. According to the induction laws of gravitomagnetism,^{12,13} such an artificial field would look like a dipole composed of gravitoelectric fields. The most straightforward propulsion concept would be to interact with the Earth's gravitational field, as outlined in Fig. 3. Such a field configuration could be used to generate a torque orienting the spacecraft parallel to the planetary gravitational field. In analogy with

Table 1 Summary of influence of gravity control and gravitoelectromagnetic propulsion on propulsion system

	F	I_{sp}	Δv	m_p/m_0	Compare with present technology
Inertial mass modification (by factor δ)	$\delta^{1/2}$	$\delta^{-1/2}$	$\delta^{-1/2}$	—	Has no influence at all
Gravitational mass Modification (by factor ε)	—	—	$\varepsilon^{1/2}$	$1 - \exp\left(-\frac{\Delta v \varepsilon^{1/2}}{v_p}\right)$	Requires very high shielding $\varepsilon \approx 0$ Electric propulsion already saves up to 90% of propellant Launch from ultrahigh tower or aircraft can save Δv too
Dipolar gravitoelectric/magnetic field	Only torque	—	—	—	Gravity booms are simple and require no power at all
Wirelike gravitomagnetic field	$<10^{-7}$ N	—	—	—	Electrodynamical tethers have much higher thrusts

**Fig. 3** Illustration of dipolar gravitoelectric/magnetic field propulsion.**Fig. 4** Illustration of wirelike gravitomagnetic field propulsion.

electromagnetism, we can write

$$\tau_g = \mu_g \times g \quad (17)$$

where τ_g is the torque, μ_g the gravitoelectric dipole momentum, and g the Earth's gravitational field. Since much simpler conventional concepts are available, we shall not elaborate further on this idea. The simplest one is the so-called gravity boom,²¹ which is used in almost all small satellites. It consists of a test mass along a deployable boom attached to the spacecraft. Due to the gravitational gradient, the boom always points the satellite toward Earth. In addition to its simplicity, such a device does not require any power at all.

We want to stress that such a dipolar gravitoelectric field is not at all a gravitational dipole, which is a mathematical object composed of a positive and negative mass. A gravitational dipole would be self-accelerating,²² however, it has been clearly shown that negative masses are forbidden in gravitational physics and that a propulsion system based on such a concept does not make sense.⁷ The impossibility of negative mass in our universe has been shown by the positive energy theorem,^{23,24} which is known to apply to all known matter in both normal and extreme cosmological situations. Violations of the energy conditions are possible in quantum theories, but the effects are fleeting and require exotic equations of state.^{25–27}

Wirelike Gravitomagnetic Field

Through the use of a "wirelike" gravitoelectric field or a gravitomagnetic field, one could generate a gravitational analog of the Lorentz force. This could be used as a propulsion system (see Fig. 4)

interacting with a planet's gravitomagnetic field. By using gravitoelectromagnetism, one can conceive a gravitational analog of an electrodynamic tether. The force F produced by a wire in a gravitational field can be expressed as

$$F = B_g/c \cdot I_m \cdot l \quad (18)$$

where B_g is the gravitomagnetic field (for Earth $B_g = 3.3 \times 10^{-14}$ rad/s), $I_m = dm/dt$ is the mass current, and l is the length of the wire. For $I_m = 3000$ kg/s (for example, by pumping liquid metal through a tube), a length of 1 km, and the Earth's gravitomagnetic field, this force is equal to $0.1 \mu\text{N}$. Comparing this unrealistic concept (huge I_m) with an electrodynamic tether used for satellites, with a typical power consumption of only 2.4 kW, a force of 0.36 N is produced in LEO. Therefore, a gravitational analog adds no extra benefit to current tether technology. Even if much larger gravitomagnetic fields than the one produced by the Earth could be produced, for example, using superconductors as proposed in Ref. 17, this conclusion does not change.

Conclusion

We can summarize our results as follows. Within the context of propulsion devices based on the reaction principle, our study reveals that control of gravity, even if achievable, would not imply a breakthrough for propulsion, even though it could be of major importance for possible microgravity applications on Earth. This is, of course, only valid for the manipulation schemes outlined. Although the manipulation schemes presented are not exhaustive, they include the most straightforward ones from the current physics point of view.

More concretely, our analysis reveals that modification of inertial mass would have no influence at all, and the modification of gravitational mass would have to compete with classical-launch assist technologies such as launching from an airplane, the top of a mountain, or in an extreme case, an ultrahigh tower. Moreover, the use of gravitomagnetic or gravitoelectric fields for propulsion would not bring any extra benefit when compared to classical electrodynamic tethers or gravity booms. Our conclusions are summarized in Table 1. We believe that the result of our analysis is a valuable input to ongoing breakthrough propulsion activities in the United States and Europe.

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